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Effect of La₂O₃ on the microstructure and electrical properties of ZnO linear resistors

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ZnO-MgO-Al₂O₃-TiO₂-Y₂O₃ linear resistors with different amount of La₂O₃ were successfully prepared by the conventional solid-state sintering method. The crystalline phase composition, microstructure, and electrical properties of La₂O₃ doped ZnO linear resistors were investigated. The results show that La₂O₃ influences the lattice of ZnO and generates La-rich phase at the grain boundaries, which improves the dense density of ZnO linear resistors. The addition of La₂O₃ further affect the electrical properties of ZnO linear resistors, such as the temperature stability. The sample with 0.5 wt.% La₂O₃ show excellent electrical performance with an resistance-temperature coefficient of 0.21×10^{-3} /°C and an nonlinear coefficient of 1.05.

Keywords: ZnO linear resistor, La2O3, Microstructure, Electrical properties.

Introduction

As an n-type semiconductor with a wide bandgap of 3.37 eV, ZnO has been widely used in solar cells [1-3], sensors [4-6], high frequency devices [7-9], photocatalysis [10-12], varistors [13-15], linear resistors [16-18] and so on. ZnO linear resistor, which has low resistancetemperature coefficient and small nonlinear coefficient, is a kind of composite resistance material with ZnO as the host material and oxides such as MgO, Al₂O₃, TiO_2 , and SiO_2 as the additives [17-22]. Compared with traditional metal and carbon based resistors, ZnO linear resistors have large flow density, adjustable resistivity, stability, and excellent resistance-temperature better characteristic [22-24]. Therefore, ZnO linear resistors have been widely used in high energy areas such as neutral grounding resistors and circuit breakers [16].

The addition of oxides is one of the most efficient way to improve the performance of ZnO linear resistances. Fe₂O₃ can be used as a donor dopant to reduce the barrier height of the grain boundary and improve the linear current-voltage (*I-V*) characteristic of ZnO linear resistors [21]. The addition of NiO into ZnO linear resistors improves the microstructure uniformity, energy density, and resistance-temperature characteristic [25]. CaO doping can limit the grain size of ZnO linear resistors, and then improve the electrical properties, including decrease the grain boundary barrier height and nonlinear coefficient, as well as optimize the resistance-temperature coefficient [26]. The doping of Sc_2O_3 enhances the linear characteristics of ZnO linear resistor, and further affects its dielectric properties [17].

In addition to the type of the doped oxides, the reactions of the doped oxides and ZnO also influence the performance of ZnO linear resistors [20, 27, 28]. The added oxides react with ZnO to produce spinel during the sintering process, which can modulate the resistance of the linear resistor and improve its resistance-temperature characteristic [22, 23]. As a rare earth oxide, La₂O₃ may react with ZnO, that is, the La³⁺ plays a donor dopant to substitute Zn²⁺ in the ZnO grains and create lattice defects [29]. On the other hand, the addition of La₂O₃ is likely to lead to La-rich phase in the ZnO linear resistors. Thus, the barrier height at the grain boundary and the resistance characteristic of ZnO linear resistor may be modulated by the doping amount of La2O3. Recent report on La2O3 doped ZnO linear resistors indicates that La2O3 doping can promote the performance of ZnO linear resistors and could enables its application in highfrequency electric field [22]. Further investigating the effect of La₂O₃ doping on ZnO linear resistors helps to better understand the mecha nism of the promoted electrical performance and further modulate its electrical properties. In our work, ZnO-MgO-Al₂O₃-TiO₂-Y₂O₃ linear resistors with different addition amounts of La_2O_3 were prepared via conventional solid-state sintering method. We studied the phase composition and microstructure of the ZnO linear resistors, and analysed the mechanism of the effect of La₂O₃ on the electrical properties of ZnO linear resistors.

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Experimental and Methods

linear resistors were fabricated ZnO through conventional solid-state sintering method with analytical grade raw materials. The mass compositions was (86.684-x) wt.% ZnO+7 wt.% Al₂O₃+5 wt.% MgO+0.6 wt.% TiO₂+0.716 wt.%Y₂O₃+x wt.% La₂O₃ (x = 0, 0.25, 0.5, 0.75 or 1). The raw materials were mixed with deionized water in a planetary ball mill at a speed of 356 r/min for 24 h. The mass ratio of powders, water, and zirconia balls was 1:3:3. The resulting slurry was dried at 100 °C for 24 h in an air dry oven. The obtained dry mixture was crashed into powders and prilled with 8 wt.% PVA, followed by aging for 24 h. The prilled powders were pressed into discs with 20 mm in diameter and 3 mm in thickness under the pressure of 10 MPa, and then the discs were sintered for 3 h at 1360 °C. Finally, after a cooling procedure (2 °C/min), the specimens were polished and coated with aluminum electrodes for further electric measurement.

The microstructure of the as-prepared specimens was observed by a scanning electron microscope (Hitachi desktop TM - 4000, Japan), and the grain size was calculated based on the linear intercept method [30]. The elemental distribution of the specimens were determined by an energy dispersive spectrometer (EDS). The crystalline phase and lattice constants of the specimens were characterized by an X-ray diffractometer (XRD, DMAX1400, Japanese physics) using Cu K α radiation ($\lambda = 0.154$ nm).

The *I-V* curves of ZnO linear resistors at 0-4 V were measured by HRMS-800 high temperature insulating material resistivity measurement system. The nonlinear coefficient of was calculated by the following equation [31]:

$$\alpha = \frac{\lg(I_2 / I_1)}{\lg(U_2 / U_1)} \tag{1}$$

where U_1 and U_2 are the voltage values at two different points of an *I-V* curve, I₁ and I₂ are the current values at the voltage of U_1 and U_2 respectively. In this paper, the obtained α is averaged over 10 data points. The resistance-temperature (*R-T*) curves of ZnO linear resistors in the temperature range of 25-300 °C were tested by HRMS-900 high temperature insulating material resistivity measurement system. The resistancetemperature coefficient is calculated by the following equation [32]:

$$\alpha_{\rm T} = \frac{\mathbf{R} - \mathbf{R}_0}{(\mathbf{T} - \mathbf{T}_0)\mathbf{R}_0} \tag{2}$$

where T_0 is the initial temperature of the test (25 °C), R_0 is the resistance of the sample at 25 °C, R is the resistance of the sample at temperature T. The calculation is averaged over 10 data points.

Results and Discussion

XRD characterization

Fig. 1 shows XRD patterns of the ZnO linear resistors with different amounts of La₂O₃ additive. The main crystalline phase compositions of the ZnO linear resistors without La₂O₃ are ZnO, ZnAl₂O₄, and MgAl₂O₄. After the addition of La₂O₃, a diffraction peak with a low intensity appears at $32^{\circ}-33^{\circ}$, and its intensity increases with the increase of La₂O₃ addition. The phase corresponding to this diffraction peak is La-rich phase [22, 33]. The enlarged XRD patterns in the range of $35-38^{\circ}$ shows that the addition of La₂O₃ leads to a leftward shift (towards the small diffraction angle) of the diffraction peak of ZnO, which means the increase of lattice parameters. This is due to the replacement of Zn²⁺ (74 pm) by La³⁺ (106 pm) during sintering. With the increase of La₂O₃ addition, the lattice parameters of



Fig. 1. XRD patterns of the ZnO linear resistors with different amount of La₂O₃.

Table 1. Lattice parameters of ZnO in ZnO linear resistors added different amounts of La_2O_3 .

| La ₂ O ₃ (wt.%) | Lattice para | 0/0 | |
|------------------------------------------|--------------|--------|--------|
| | a=b | с | C/a |
| 0 | 3.2461 | 5.1818 | 1.5963 |
| 0.25 | 3.2542 | 5.1944 | 1.5962 |
| 0.5 | 3.2545 | 5.1976 | 1.5970 |
| 0.75 | 3.2546 | 5.1995 | 1.5976 |
| 1 | 3.2534 | 5.1924 | 1.5960 |

ZnO increase first and then decrease, as shown in Table 1. When the addition of La_2O_3 is 0.75 wt.%, the lattice parameters of ZnO reach the maximum. Further increasing La_2O_3 to 1 wt.% decreases the lattice parameters of ZnO. This may be due to the fact that when too much La_2O_3 is added, it is more likely to segregate at the grain boundaries and resulting in less La^{3+} entering the ZnO lattice.

Bulk density

The bulk density and relative density of the samples with different different amounts of La_2O_3 are shown in Fig. 2. The density of the samples increases with the increase of La_2O_3 addition, and slightly decreases when the addition of La_2O_3 is greater than 0.75 wt.%. When the addition of La_2O_3 is 0.75 wt.%, the bulk density and relative density of the ZnO linear resistors are 5.040 g/cm³ and 95.27% respectively, which are the maximum values of these samples. The slightly increased density of the samples with the addition of La_2O_3 is because La_2O_3 has the effect of activating the lattice [22]. However, when the La_2O_3 addition is 1 wt.%, the segregation of the La-rich phase at the grain boundaries affects the homogeneity of ZnO [29] and cause the



Fig. 2. The bulk density and relative density of ZnO linear resistors with different amount of La_2O_3 .

decrease of density.

Microstructure characterization

To understand the impact of the La_2O_3 on the microstructure, we observed the morphology of the samples with different amounts of La_2O_3 by SEM, as shown in Fig. 3. Without the addition of La_2O_3 , the ZnO grains are irregularly slender in shape. With the increase of La_2O_3 addition, a new phase (bright areas in Fig. 3(c-e)) appeared, which may be La-rich phase that manifested in XRD patterns. Moreover, the ZnO grain size increases with the increase of La_2O_3 addition of 0.75 wt.% (as summarized in Table 2). When the addition of La_2O_3 is 0.75 wt.%, the ZnO grain size is significantly refined and uniformly distributed.

During the sintering process, atoms diffuse along the grain boundaries, causing migration of grain boundaries



Fig. 3. SEM images of ZnO linear resistors with different amount of La_2O_3 . (a) without La_2O_3 , (b) 0.25 wt.% La_2O_3 , (c) 0.5 wt.% La_2O_3 , (d) 0.75 wt.% La_2O_3 , and (e) 1 wt.% La_2O_3 .

Table 2. Average grain size of ZnO linear resistors with different amounts of La_2O_3 .

| La ₂ O ₃ (wt.%) | 0 | 0.25 | 0.5 | 0.75 | 1 |
|---------------------------------------|------|------|------|------|------|
| Average grain sizes (μm) | 3.33 | 3.66 | 3.75 | 2.67 | 3.72 |

and growth of grains [34, 35]. The migration of grain boundaries is determined by the distribution of the second phase at the grain boundaries and the defects in other regions. The effect of La_2O_3 on the microstructure of ZnO linear resistors is mainly manifested in two ways: (1) La^{3+} distributes at the grain boundaries and activates the migration of grain boundaries, leading to the growth of ZnO grains; (2) La^{3+} enters the lattice of ZnO by substituting Zn^{2+} [29], which inhibit the migration of grain boundaries and the growth of grains. When the amount of La_2O_3 is small, La^{3+} ions mainly distribute at the grain boundaries, which results in the increase of grain size. However, with the increase of La_2O_3 , more La^{3+} ions enter the lattice of ZnO and



Fig. 4. EDS characterization of ZnO linear resistor without addition of La_2O_3 . (a) SEM image, (b)-(g) element mappings of Zn, O, Ti, Y, Al, and Mg. (h) and (i) show the energy dispersive spectra of the ZnO grain (position 1) and spinel phase (position 2), respectively.

| | | | (a) Mg | | | (b) Y | | (C) | | 0 | (d) |
|-----------------------------------------|----------------------------------|---------------------|--------------|----------------------|----------|-------|-------|---------|-------|-----|---------|
| | | Part of | | Al | | (e) | Zn | | (f) | Ti | (g) |
| pt-doorcoot 156V e Brim X Spectrum 3 | 5.00k BSE H 09/1 | 0.202 (09.28 (i) | tò.oµm Sp | ectrum 4 | | (j) |) (k) | Spectru | m 5 | La | (h) |
| Elemen | t Wt.% | | | Element | Wt.% | | | Element | Wt.% | | |
| 0 | 12.26 | | | 0 | 17.14 | | | 0 | 19.59 | 4 | |
| Mg | 2.34 | | | Mg | 3.08 | | | Mg | 2.81 | | |
| Al | 1.28 | | | Al | 19.57 | | | Al | 15.99 | 0.3 | 18. E 4 |
| Ti | 0.18 | | | Ti | 0.66 | | | Ti | 0.82 | | |
| Zn | 82.76 | | + + | Zn | 58.06 | | | Zn | 58.22 | | |
| Y | 0.8 | | | Y | 0.71 | | | Y | 0.68 | | |
| LaLa | 0.38 | | | La | 0.78 | | | La | 1.9 | _ | |
| il trois , t. | te 10 fa fa fa 11 fa fa fa | 1.1 | in a la sine | 5 150 10 20 10 10 | 14 14 | 1 | i iii | i vin | | | 1. 1 |

Fig. 5. EDS characterization of ZnO linear resistor with 0.75 wt.% La_2O_3 . (a) SEM image, (b)-(h) element mappings of Mg, Y, O, Al, Zn, Ti, and La. (i)-(k) show the energy dispersive spectra of the ZnO grain (position 3), spinel phase (position 4), and La-rich phase (position 5), respectively.

inhibit the growth of grains.

To further determine the phase composition of the ZnO linear resistors, we performed EDS measurements. Fig. 4 and Fig. 5 show the EDS results of ZnO linear resistors without and with 0.75 wt.% La₂O₃, respectively. According to the element mappings and element ratios results, the sample without addition of La₂O₃ is mainly composed of ZnO (light grey areas) and spinel phase (dark grey areas). In the sample with $0.75 \text{ wt.}\% \text{ La}_2\text{O}_3$, La element is mainly distributed at the grain boundaries and formed the La-rich phase (bright areas). In addition, the aggregation of Ti element at the grain boundaries in the sample with 0.75 wt.% La₂O₃ is significantly enhanced compared with the sample without addition of La₂O₃. Ti element can enter the ZnO lattice and promote the growth of grain [16]. The aggregation of Ti element at the grain boundaries indicate that there is less Ti in ZnO lattice, which may be a reason that cause the refinement of ZnO grains in the sample with 0.75 wt.% La₂O₃.

Electrical properties

It is critical to know the electrical properties of La₂O₃ doped ZnO linear resistors, such as the resistivity, resistance-temperature coefficient, and nonlinear coefficient of the samples. Fig. 6 shows the resistance and resistivity of ZnO linear resistors with different amounts of La₂O₃. The resistance and resistivity of ZnO linear resistors decrease significantly with the increase of La_2O_3 . The resistance (resistivity) values of the sample without addition of La₂O₃ is 16.12 Ω (137.18 Ω ·cm), and the resistance (resistivity) values of the sample with 1 wt.% La₂O₃ is decreased to 3.95 Ω (32.76 Ω ·cm). The resistance of ZnO linear resistors is determined by both the low resistance ZnO grain and the high resistance grain boundary phase. The addition of La₂O₃ not only affects the grain boundaries, but also reduces the resistance of ZnO grains because La³⁺ enter the lattice of ZnO can increase the concentration of free



Fig. 6. Resistance and resistivity of ZnO linear resistors with different amount of La_2O_3 .

electrons [29]. As a result, the resistance and resistivity of ZnO linear resistors decreases with the addition of La_2O_3 .

The resistance-temperature coefficients of the ZnO linear resistors are shown in Fig. 7. The absolute values of the ZnO linear resistors with different amounts of La₂O₃ were reduced to smaller than 10^{-3} /°C, which indicate that the addition of La₂O₃ improves the temperature stability of the ZnO linear resistors noticeably. When the addition of La₂O₃ is 0.5 wt.%, the sample has the best temperature stable performance with a resistance-temperature coefficient of 0.21×10^{-3} /°C. The improvement of the temperature stable performance of ZnO linear resistors is because the added La₂O₃ influenced the grain boundaries and promoted the conductance of ZnO.

Fig. 8 shows the nonlinear coefficient of ZnO linear resistors with different amounts of La_2O_3 . The addition of La_2O_3 increases the nonlinear coefficient of the samples except the sample with 0.5 wt.% La_2O_3 . We further analysed the temperature dependent resistivity according to the thermally activated conduction mechanism



Fig. 7. Resistance-temperature coefficient of ZnO linear resistors with different amount of La_2O_3 .



Fig. 8. Nonlinear coefficient of ZnO linear resistors with different amount of La₂O₃.



Fig. 9. Arrehenius plots of the temperature dependent resistivity of ZnO linear resistors with different amount of La_2O_3 . (a) without La_2O_3 , (b) 0.25 wt.% La_2O_3 , (c) 0.5 wt.% La_2O_3 , (d) 0.75 wt.% La_2O_3 , and (e) 1 wt.% La_2O_3 .

because the electrical transport in semiconductor ceramics is thermally activated. The resistivity of ZnO linear resistors can be expressed as [17, 22]

$$\rho = \rho_0 e^{(\phi_0/kT)} \tag{3}$$

where ρ is the resistivity of the sample, ρ_0 is the resistivity of the sample as the temperature tends to infinity; φ_0 is the height of the grain boundary potential barrier (equal to value of the activation energy), *k* is the Boltzmann constant, and *T* is the absolute temperature. The Arrhenius plots of the temperature dependent resistivity of ZnO linear resistors are shown in Fig. 9. We linearly fitted the relationship between $\ln\rho$ and 1000/T and obtained the height of the grain boundary potential barrier by calculating the slops. Here, all the coefficient of determination (R²) are greater than 0.98,

indicating that the electrical transport in ZnO linear resistors matches the thermally activated conduction mechanism well. The addition of La₂O₃ increases φ_0 obviously except the sample with 0.5 wt.% La₂O₃, which is consistent with the trend of nonlinear coefficient. This indicate that the nonlinearly electrical characteristic of La₂O₃ doped ZnO linear resistors is determined by the grain boundary potential barrier, which is adjusted by the addition of La₂O₃.

The potential barrier height φ_0 is expressed by the following equation [17, 22]:

$$\varphi_0 = \frac{e^2 N_s^2}{2 N_d \varepsilon_0 \varepsilon} \tag{4}$$

where e is the elementary charge, $N_{\rm S}$ is the density of

interfacial state, N_d is the donor density, ε is relative dielectric constant, and ε_0 is the vacuum dielectric constant. When La₂O₃ is added into ZnO linear resistors, some of the La³⁺ ions enter ZnO lattice to increase the donor density N_d and decrease φ_0 ; the other La³⁺ ions distribute at the grain boundaries to generate La-rich phase, which increase the density of interfacial state N_s and thus increase φ_0 . Because ionic radius of La³⁺ (106 pm) is much greater than that of Zn²⁺ (74 pm), the amount of La³⁺ ions that entering ZnO lattice is limited and most of the La³⁺ ions are distribute at the grain boundaries to generate La-rich phase. As a result, the height of the grain boundary potential barrier is increased and the nonlinearity of the *I-V* curves also increased.

Due to the complicated components of La_2O_3 doped ZnO linear resistors, all the main crystalline phases, including ZnO, spinel phase, and La-rich phase, can affect the grain boundary potential barrier and charge transport, which makes the factors that affect their electrical conductance quite complex. Thus, more researches are needed in the future to better understand the resistance-temperature characteristic and *I-V* characteristic.

Conclusions

ZnO-MgO-Al₂O₃-TiO₂-Y₂O₃ linear resistors doped with different amount of doping were prepared through the conventional solid-state sintering method, and the effect of La₂O₃ on the microstructure and electrical properties of these resistors was investigated. The addition of La₂O₃ increased the lattice constant of ZnO due the substitution of La³⁺ for Zn²⁺, and generated Larich phase at the grain boundaries due to the reaction between La₂O₃ and the components of ZnO linear resistor. As a result, the addition of La₂O₃ modulated the grain boundary potential barrier and improved the temperature stability of ZnO linear resistors. The sample with 0.5 wt.% La₂O₃ showed excellent resistancetemperature characteristic with an resistance-temperature coefficient of 0.21×10⁻³/°C, and good linear I-V characteristic with an nonlinear coefficient of 1.05. This work indicates that the doping of rare earth oxides may modulate the microstructure and hence benefits the performance improvement of ZnO based linear resistors.

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Declarations:

Conflict of interest: the authors declare that there are no conflicts of interest.

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