# Homogeneous distribution and quantitative evaluation of sintering additives in spray-dried silicon nitride granules 

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#### Abstract

Quantitative phase evaluation of sintering additives and their homogeneous distribution in ceramics are critical issues in ceramic processing. In the present work, we report the characteristics of silicon nitride granules containing sintering additives $\left(\mathrm{Y}_{2} \mathrm{O}_{3}-\mathrm{Al}_{2} \mathrm{O}_{3}-\mathbf{Y b}_{2} \mathrm{O}_{3}\right.$ ) prepared by spray drying. For homogeneous mixing of sintering additives, using fine and similar particle sizes for all sintering additives is essential. In this study, the particle size was reduced by ball milling based on the particle size of the as-received sintering additive. Systematic studies using scanning electron microscopy and particle size analysis were conducted on starting materials and spray-dried granules. Highly stable aqueous slurries consisting of $\mathbf{2 5} \mathbf{v o l} \%$ of silicon nitride particles, $5 \mathrm{wt} . \%$ sintering additives, and $0.5 \mathrm{wt} . \%$ each of dispersant, binder, and plasticizer, were used in preparing the granules. Quantitative phase analysis and homogenous distribution of sintering additives in the granules were assessed by examining the mixing index values through Rietveld analysis of X-ray diffraction data and energy dispersive X-ray spectroscopy studies.


Keywords: Ceramics, Silicon nitride, Microstructure, Spray drying, Granules.

## Introduction

Silicon nitride $\left(\mathrm{Si}_{3} \mathrm{~N}_{4}\right)$ is one of the most attractive advanced ceramic materials used in many engineering applications due to its excellent properties [1,2]. However, sintering $\mathrm{Si}_{3} \mathrm{~N}_{4}$ is very difficult at relatively low temperatures; therefore, sintering additives are necessary in terms of densification. Accordingly, many sintering additives, including single- and multi-component $\mathrm{Al}_{2} \mathrm{O}_{3}, \mathrm{Y}_{2} \mathrm{O}_{3}$, and $\mathrm{Yb}_{2} \mathrm{O}_{3}$, have been evaluated as being more efficient [3-6].
Although several studies have reported the preparation of different $\mathrm{Si}_{3} \mathrm{~N}_{4}$ materials with desired morphologies using different methods and various sintering additives, these studies have focused primarily on the processing methods [7-13]. Granule morphological silicon nitrides with controlled particle sizes have attracted considerable attention from various ceramic industries because of their ease of handling for numerous applications [1417]. Spray drying is one of the most convenient ceramicforming methods used in the granulation of ceramic materials. Spray drying is a simple and economically feasible method to produce ceramic granules [18-21].

However, studies on the fabrication of silicon nitride granules with sintering additives are limited [14, 17]. Some studies have been conducted, but research on the control of processing parameters for granule preparation,

[^0]quantitative analysis, and evaluation of the homogenous distribution of sintering aids is lacking. Therefore, in the present study, we aimed to understand the characteristics of silicon nitride granules containing sintering additives (2.4 wt. $\% \mathrm{Y}_{2} \mathrm{O}_{3}+1.6 \mathrm{wt} . \% \mathrm{Al}_{2} \mathrm{O}_{3}+$ $1 \mathrm{wt} . \% \mathrm{Yb}_{2} \mathrm{O}_{3}$ ) prepared by spray drying.

## Materials and Methods

Commercially available high-purity $\mathrm{Si}_{3} \mathrm{~N}_{4}$ (E-10, Ube, Japan) was used as a raw material. High-purity $\mathrm{Al}_{2} \mathrm{O}_{3}$ (AES-11C, Sumitomo, Japan), $\mathrm{Y}_{2} \mathrm{O}_{3}$ (Wonik, South Korea), and $\mathrm{Yb}_{2} \mathrm{O}_{3}$ (Wonik, South Korea) were used as sintering additives. The average particle sizes of the as-received silicon nitride, alumina, yttria, and ytterbium powders were approximately $0.9,0.73,0.67$, and $3.18 \mu \mathrm{~m}$, respectively. To maintain similar fine and micron-sized particles of all sintering additives for better mixing, ytterbium oxide was ball-milled to reduce the particle size to approximately $0.68 \mu \mathrm{~m}$. The as-received silicon nitride, alumina, yttria, and reduced ytterbium oxide powders were thoroughly ball-milled for 12 h using $5-\mathrm{mm} \mathrm{Si}_{3} \mathrm{~N}_{4}$ balls after adding $0.5 \mathrm{wt} . \%$ ammonium polymethacrylate (Darvan C, R.T. Vanderbilt Co. Inc., USA) as a dispersant, polyethylene glycol (PEG400, Daejung Chemicals, South Korea) as a plasticizer, and polyvinyl alcohol (PVA 205, Daejung Chemicals, South Korea) as a binder in deionized water to each material to ensure homogeneous mixing of all phases in the slurry. A solid loading of $25 \mathrm{vol} . \%$ was used in the slurry. Sintering additives of $5 \mathrm{wt} . \%$ in

Table 1. Operating spray-drying conditions used in the present work.

| Atomizer $(\mathrm{kPa})$ | 5 |
| :--- | :---: |
| Pump $(\mathrm{mL} / \mathrm{h})$ | 450 |
| Inlet temperature $\left({ }^{\circ} \mathrm{C}\right)$ | 140 |
| Outlet temperature $\left({ }^{\circ} \mathrm{C}\right)$ | 80 |
| Blower $\left(\mathrm{m}^{3} / \mathrm{min}\right)$ | 0.37 |
| Granule size $\left(\mathrm{D}_{50}, \mu \mathrm{~m}\right)$ | 27.4 |
| $\mathrm{~W}_{\text {psd }}$ | 1.93 |

the ratio of $2.4 \mathrm{wt} . \% \mathrm{Y}_{2} \mathrm{O}_{3}+1.6 \mathrm{wt} . \% \mathrm{Al}_{2} \mathrm{O}_{3}+1 \mathrm{wt} . \%$ $\mathrm{Yb}_{2} \mathrm{O}_{3}$ were added. After ball milling, the stability of the slurry was assessed by examining the zeta potential behavior using a zeta potential analyzer (ELSZ-200, Otsuka, Japan). The sedimentation behavior was also examined. The surface areas of the ball-milled powders after drying were determined using a BET analyzer (BELSORP-max, Japan). After degassing, the highly stable slurry was spray-dried using a spray drier (EYELA, SD-1000). The operating conditions of the spray drier are presented in Table 1. To prevent sedimentation, the slurries were mixed rigorously throughout the spray-drying period. The particle sizes of the raw powders, ball-milled powders, and granules were investigated using a laser diffraction particle size analyzer (PSA, Mastersizer 2000, Malvern, England). X-ray diffraction (XRD, SWXD(D-MAX/2500-PC), Rigaku, Japan) was performed in a range of $10^{\circ}-70^{\circ} 2 \theta$ to analyze the phase purity and crystal structures at room temperature. The Fullprof program was used for Rietveld analysis of the XRD data [22]. The microstructures were characterized and energy-dispersive Xray spectroscopy elemental mapping studies of the granules were conducted using scanning electron microscopy (SEM, JSM-6500F, JEOL, Japan).

## Results and Discussion

Fig. 1 shows SEM micrographs of the as-received $\mathrm{Y}_{2} \mathrm{O}_{3}, \mathrm{Al}_{2} \mathrm{O}_{3}$, and ball-milled $\mathrm{Yb}_{2} \mathrm{O}_{3}$ sintering additives used in this study. The SEM micrograph of the asreceived silicon nitride raw powder is also compared in Fig. 1. For homogeneous mixing of sintering additives in silicon nitride granules, using similar particle sizes for all sintering additives is essential. Because in this study the particle sizes of the as-received sintering additives were different, ball milling was performed based on the sizes of the particles. Irregular particle sizes of sintering additives may lead to inhomogeneous mixing; therefore, $\mathrm{Yb}_{2} \mathrm{O}_{3}$ was initially milled to reduce the particle size. Fig. 1 shows that all powders exhibited similar particle sizes of approximately $1 \mu \mathrm{~m}$. These results were corroborated by the PSA graphs shown in Fig. 1(e). After the powders containing silicon nitride and sintering additives were ball-milled for 12 h , the


Fig. 1. SEM micrographs of as-received (a) $\mathrm{Si}_{3} \mathrm{~N}_{4}$, (b) $\mathrm{Y}_{2} \mathrm{O}_{3}$, (c) $\mathrm{Al}_{2} \mathrm{O}_{3}$, and (d) ball-milled $\mathrm{Yb}_{2} \mathrm{O}_{3}$ powders, (e) PSA graphs of sintering additives.
powders achieved an average particle size of approximately $0.62 \mu \mathrm{~m}$, as indicated by their PSA behaviors (Fig. 2), and a high surface area of $11.5 \mathrm{~m}^{2} / \mathrm{g}$, as evidenced by BET analysis. Subsequently, the stability of the aqueous slurries containing sintering additives and silicon nitride powders was evaluated. For this purpose, a dispersant, binder, and plasticizer were added,


Fig. 2. Comparison of PSA behaviors of $\mathrm{Si}_{3} \mathrm{~N}_{4}$ powders with and without sintering additives (SA).


Fig. 3. Digital camera images of sedimentation behaviors of slurries after ball-milling for 12 h .
and both zeta potential and sedimentation studies were performed. Zeta potential measurements indicated a high value of -40 mV at pH 9 , and sedimentation results indicated that the slurries were highly stable for at least 48 h at this pH , as shown in Fig. 3.
After the slurry containing sintering additives and silicon nitride powders was prepared under optimal conditions, a spray dryer was used to produce granules with average particle sizes of approximately $\mathrm{D}_{50} 27.4$ $\mu \mathrm{m}$, as evidenced by the PSA graph (Fig. 4). Typical SEM images of $\mathrm{Si}_{3} \mathrm{~N}_{4}$ granules at different magnifications, along with their elemental mappings, are presented in


Fig. 4. Typical PSA behavior of $\mathrm{Si}_{3} \mathrm{~N}_{4}$ granules.


Fig. 5. SEM micrographs of spray-dried $\mathrm{Si}_{3} \mathrm{~N}_{4}$ granules at different magnifications and its elemental mapping.

Fig. 5. The images show that the granules were dense and exhibited circular shapes with an average size of approximately $30 \mu \mathrm{~m}$. The homogeneous distribution of $\mathrm{Si}, \mathrm{Y}, \mathrm{Al}$, and Yb could also be observed from the EDS elemental mapping analytical images, which indicated that all the sintering additives were distributed homogeneously in the granules. Quantitative analysis was performed by evaluating the degree of mixing index for granules using the following goodness-of-fit method, where Eq. (1) considers the wt. $\%$ of metallic elements from EDS data.

$$
\begin{equation*}
\chi^{2}=\sum_{i=1}^{k} \frac{\left(O_{i}-E_{i}\right)^{2}}{E_{i}}, \tag{1}
\end{equation*}
$$

Here, $\mathrm{O}_{\mathrm{i}}$ is the $\mathrm{i}^{\text {th }}$ observed value (experimental) and $\mathrm{E}_{\mathrm{i}}$ is the $i^{\text {th }}$ expected value (theoretical). EDS data was analyzed by considering a minimum of 30 data locations (on at least 10 granules three times each). The results indicated a good mixing index value of approximately 0.1 .

To investigate the crystal structures and evaluate quantitatively the different phases present in the granules, Rietveld refinement was performed for the XRD data using the Fullprof method. Rietveld refinement is a powerful and convenient technique used for quantitative phase analysis that relies on the intensities of XRD data. Fig. 6 presents the Rietveld refinement analysis of the granules. The XRD data clearly show the presence of peaks only for the anticipated $\mathrm{Si}_{3} \mathrm{~N}_{4}, \mathrm{Y}_{2} \mathrm{O}_{3}, \mathrm{Al}_{2} \mathrm{O}_{3}$, and $\mathrm{Yb}_{2} \mathrm{O}_{3}$ phases. No impurity peaks were detected. Fig. 6 also shows good agreement between the XRD patterns of the observed and calculated data. The difference data, along with Bragg's positions for all the phases, are also presented in the figure. All quality


Fig. 6. Typical Rietveld analysis of $\mathrm{Si}_{3} \mathrm{~N}_{4}$ granules containing sintering additives.
factors obtained in this study were found to be very low $\left(R_{p}=1.62, R_{w p}=2.06\right.$, and $\left.R_{\exp }=0.95\right)$, indicating reliable fitting. The quantitative weight fractions (wt.\%) from Rietveld analysis for the $\mathrm{Si}_{3} \mathrm{~N}_{4}, \mathrm{Y}_{2} \mathrm{O}_{3}$, $\mathrm{Al}_{2} \mathrm{O}_{3}$, and $\mathrm{Yb}_{2} \mathrm{O}_{3}$ phases were found to be $95.17 \%$, $2.35 \%, 1.56 \%$, and $0.92 \%$, respectively. These values were in good agreement with the initial amounts of added powders. A good mixing index value of less than 0.09 was achieved from the goodness-of-fit analysis from (1), which corroborated the EDS data. The average Rietveld analysis of five samples of wt.\% data was considered for the mixing index evaluation.
Based on the above results, it can be concluded that other required ceramic granules could be easily fabricated industrially at larger scale in a similar way. Although several studies have reported the preparation of different $\mathrm{Si}_{3} \mathrm{~N}_{4}$ materials with desired morphologies using different methods and various sintering additives, these studies have focused primarily on the processing methods [7-14]. However, studies on the fabrication of silicon nitride granules with sintering additives are limited. Some studies have been conducted, but research on the control of processing parameters for granule preparation, quantitative analysis, and evaluation of the homogenous distribution of sintering aids is lacking. The present study aimed at the quantitative phase evaluation of sintering additives and their homogeneous distribution, which are critical issues in ceramic processing. To achieve homogeneous mixing of sintering additives in granules, using fine and similar particle sizes for all sintering additives is essential. In this study, the particle size was reduced by ball milling based on the particle sizes of the starting powders. Quantitative phase analysis and homogenous distribution of sintering additives in the granules were assessed by examining the mixing index values through Rietveld analysis of X-ray diffraction data and energy dispersive X-ray spectroscopy studies. Results indicated good
mixing of the sintering additives. To investigate the crystal structures and evaluate quantitatively the different phases present in the granules, Rietveld refinement was performed for the XRD data using the Fullprof method. Because in this study the particle sizes of the asreceived sintering additives were different, ball milling was performed based on the sizes of the particles. Irregular particle sizes of sintering additives may lead to inhomogeneous mixing.

## Conclusions

To achieve homogeneous mixing of sintering additives in granules, using fine and similar particle sizes for all sintering additives is essential. In this study, the particle size was reduced by ball milling based on the particle sizes of the starting powders. Silicon nitride granules were prepared using highly stable aqueous slurries consisting of $25 \mathrm{vol} . \%$ of silicon nitride particles, 5 $\mathrm{wt} . \%$ sintering additives, and $0.5 \mathrm{wt} . \%$ each of dispersant, binder, and plasticizer. Quantitative phase analysis and homogenous distribution of sintering additives in the granules were assessed by examining the mixing index values through Rietveld analysis of X-ray diffraction data and energy dispersive X-ray spectroscopy studies. Results indicated good mixing of the sintering additives. Based on the results, it can be concluded that other required ceramic granules could be fabricated industrially at larger scale using the similar processing technique. Further studies on the effects of various sintering conditions on the prepared silicon nitride granules are necessary, which are in progress.

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Conflicts of interest: The authors declare no competing financial interest.

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