

## The role of La content on microstructure and magnetic characteristics of the $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$ hexagonal ferrites

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Hexagonal ferrites  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  magnetic powders and magnets were prepared by the solid state reaction. The phase compositions of the magnetic powders were identified by X-ray diffraction. There is a single magnetoplumbite phase in the magnetic powders with  $x$  from 0.12 to 0.32, and for the magnetic powders with  $x \geq 0.36$ , the  $LaFeO_3$  phase is observed. The microstructures of the magnets were investigated by a field emission scanning electron microscopy. The magnets are formed of hexagonal-shaped crystals and the particles are distributed homogeneously. The magnetic properties of the magnets were measured by a magnetic properties test instrument. The remanence of the magnets increases with  $x$  from 0.12 to 0.40. However, the intrinsic coercivity, magnetic induction coercivity and maximum energy product of the magnets first increase with  $x$  from 0.12 to 0.24, and then begin to decrease when  $x$  continues to increase.

**Key words:** M-type hexaferrites, La content, La-Cu substitution, Magnetic properties.

### Introduction

The hexagonal ferrites  $(Ba, Sr)Fe_{12}O_{19}$  have been widely used in applications such as permanent magnets, microwave devices, magneto-optics and magnetic recording media due to their low cost, excellent chemical stability and corrosion resistance [1, 2]. In order to obtain magnetic materials with the appropriate remanence and coercivity, adding or doping some elements were widely used. Several studies on hexagonal ferrites of substitution of Sr ions with different cations, such as  $La^{3+}$ ,  $Pr^{3+}$ ,  $Nd^{3+}$  and  $Sm^{3+}$  [3-6]. Several studies on hexagonal ferrites in which Fe ions are substituted by different cations have been carried out to obtain the hexagonal ferrites with appropriate magnetic properties. Among the investigated substitutions are  $Co^{2+}$ ,  $Cr^{3+}$ ,  $Ti^{4+}$ ,  $Al^{3+}$  and  $Sn^{4+}$  [7-11]. The hexagonal ferrites with combined substitution such as La-Co, La-Zn, La-Cu, Co-Ti and La-CoZn have been reported [12-17].

Although Qiao et al. [14] and Yang et al. [15] have reported the influence of La-Cu substitution on magnetic properties of strontium hexaferrites, the effects of La content on the microstructure and magnetic characteristics of La-Cu substituted strontium hexaferrites have been rarely investigated. In the present paper, the hexaferrite  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  magnetic powders and magnets were synthesized by the solid state reaction. The role of La content ( $x$ ) on the microstructure and magnetic characteristics of the  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  hexagonal ferrites has been studied systematically.

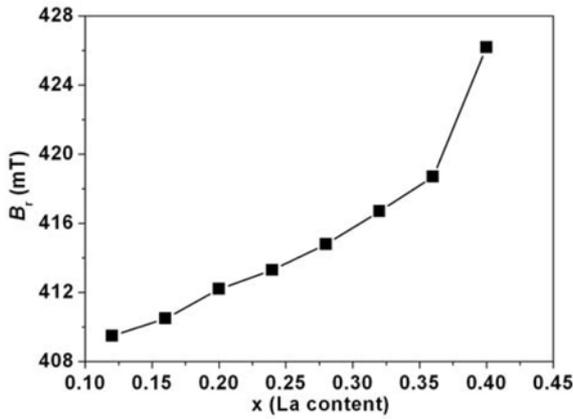
### Experimental Procedure

The hexaferrite  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  magnetic powders and magnets were prepared according to the solid state reaction. The starting materials used in this study were  $SrCO_3$  (99% purity),  $La_2O_3$  (99% purity),  $Fe_2O_3$  (99% purity) and  $CuO$  (99% purity), mixed together in the nominal composition of  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$ , where the La content ( $x$ ) varies from 0.12 to 0.40 with about 0.04 increment. Mixtures of the starting materials were milled in water for 8 hours with an angular velocity of 80 rpm and a ball-to-power weight ratio of 12 : 1. The milling processes were performed in a ball mill using hardened steel balls (diameter 8 mm). The mixed power was dried, crushed, and sifted. The sifted powders were made into balls (diameter about 8 mm), and the temperature was increased up to 1250 °C in a laboratory furnace; and then these balls were calcined for 2 hours in air atmosphere. The calcined balls were shattered to particles less than 100  $\mu m$  using a vibration mill, then wet-milled with additives ( $CaCO_3$ ,  $SiO_2$ ,  $Al_2O_3$  and  $H_3BO_3$ ) for 14 hours using a ball-mill. The finely milled slurry with a diameter of about 0.75  $\mu m$  was pressed into disc-shaped pellets (diameter 8 mm, thickness 15 mm) under 310 MPa in the magnetic field of 900 kA/m, which was parallel to the pressing direction. The green pellets were sintered in a laboratory furnace at 1180 °C for 1.5 hours in air atmosphere.

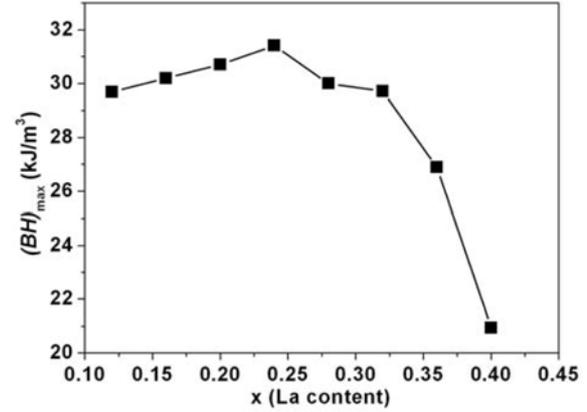
The phase compositions of the magnetic powders were determined using a PANalytical X'Pert Pro diffractometer in continuous mode with  $Cu K_{\alpha}$  ( $\lambda = 1.5406 \text{ \AA}$ ) radiation. The micrographs of the magnets were observed using a HITACHI S-4800 field emission scanning electron microscopy (FESEM). The magnetic properties of the

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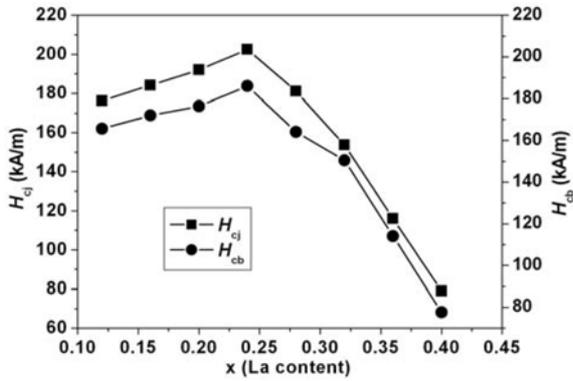




**Fig. 3.** The remanence ( $B_r$ ) of the hexaferrite  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  magnets as a function of La content ( $x$ ).



**Fig. 5.** The maximum energy product  $[(BH)_{max}]$  of the hexaferrite  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  magnets as a function of La content ( $x$ ).



**Fig. 4.** The intrinsic coercivity ( $H_{cj}$ ) and magnetic induction coercivity ( $H_{cb}$ ) of the hexaferrite  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  magnets as a function of La content ( $x$ ).

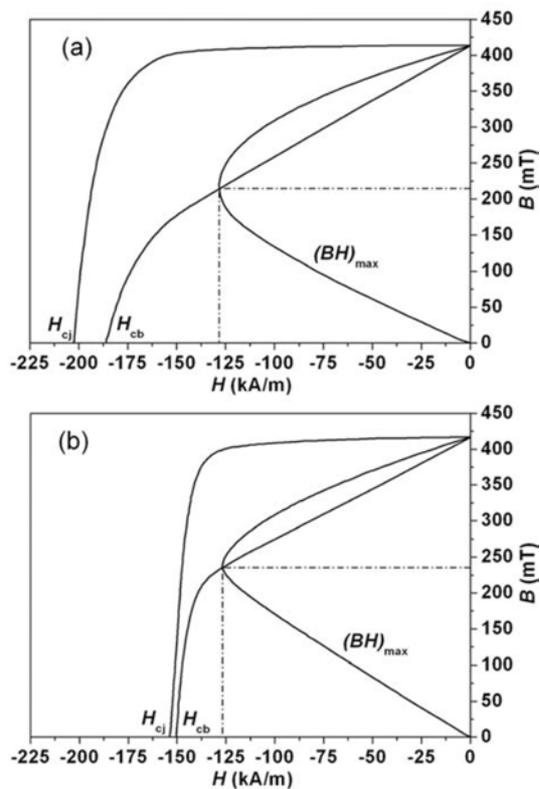
interaction at 2b and 12k sites, as reported in previous works [3, 19]. When the La content ( $x$ ) is increased from 0.12 to 0.40, the lattice parameter  $c$  decreases as shown in Table 1. And then, the  $Fe^{3+}-O^{2-}$  distance that is parallel to the  $c$ -axis decreases, which will cause the  $Fe^{3+}-O-Fe^{3+}$  superexchange interaction strength to increase. This results in an increase in the hyperfine fields at 2b and 12k sites.

Fig. 4 shows the influence of La content ( $x$ ) on the intrinsic coercivity ( $H_{cj}$ ) and magnetic induction coercivity ( $H_{cb}$ ) of the hexaferrite  $Sr_{1-x}La_xFe_{11.80}Cu_{0.20}O_{19}$  magnets. As seen from the figure,  $H_{cj}$  and  $H_{cb}$  of the magnets first increases from 176.2 and 165.6 kA/m (at  $x=0.12$ ) to 202.5 and 186.0 kA/m (at  $x=0.24$ ), respectively. With a further increase in the La content ( $x$ ),  $H_{cj}$  and  $H_{cb}$  decreases drastically, and reach to 78.9 and 77.6 kA/m at  $x=0.40$ . The change of the coercivity with La content is in agreement with that reported by Liu et al.<sup>3</sup> and Wang et al. [20]. The coercivity of the magnets depends both on their magnetocrystalline anisotropy and on their microstructure. According to the literature [21], the coercivity can be described by the following expression:

$$H_c = aH_a - \frac{N(B_r + J_s^0)}{\mu_0} \quad (2)$$

where  $\alpha$  is the microstructure factor,  $N$  is the grain demagnetization factor,  $H_a$  is the magnetocrystalline anisotropy field, and  $J_s^0$  is the saturation polarization of the magnet. The factor  $\alpha$  increases with decreasing grain size, thus reflecting the well-known  $H_c$ -grain size dependency; the factor  $N$  is govern by the grain shape and increases when the grain shape becomes more platelet shaped. The representative FESEM micrographs shown in Fig. 2 exhibit that the mean particle size and particle morphology of the magnets do not change basically with the increase of  $x$ , which implies that the factors  $\alpha$  and  $N$  remain constant. Therefore, it can be concluded that the increase of  $H_{cj}$  and  $H_{cb}$  with increasing  $x$  from 0.12 to 0.24 can be due to the magnetocrystalline anisotropy field increase with increasing La content. As the content of  $La^{3+}$  increases, the  $Fe^{3+}$  ions present at octahedral sites are forced to migrate towards the tetrahedral sites. It leads to the conversion of  $Fe^{3+}$  (high spin) into  $Fe^{2+}$  (low spin) to maintain the electrical neutrality of M-type hexaferrite. The formation of any low spin iron ions on the tetrahedral site during processing, preferentially occupy 2a octahedral site [22]. As a result, the number of  $Fe^{2+}$  ions on octahedral site increases with increasing La content. The  $Fe^{2+}$  ions enhance the coercivity due to strong magnetocrystalline anisotropy of  $Fe^{2+}$  on 2a sites [22, 23]. And this leads to an increase in coercivity. On the other hand, the decrease of  $H_{cj}$  and  $H_{cb}$  with increasing  $x$  from 0.24 to 0.40 can be attributed to two factors. The first factor is that an increase in the abundance of  $Fe^{2+}$  ions, which arises with increasing  $x$ , will destroy the regular atomic arrangement of the  $Fe^{3+}$  ions, and this results in a decrease in coercivity [24]. The second one is that the amount of magnetic impurities such as the  $LaFeO_3$  phase which will destroy the regular atomic arrangement of the  $Fe^{3+}$  ions increases with the increase of  $x$  shown in Fig. 1, which leads to a reduction in coercivity [20].

The influence of La content ( $x$ ) on the maximum energy product  $[(BH)_{max}]$  of the hexaferrite  $Sr_{1-x}$



**Fig. 6.** Typical demagnetizing curves for the hexaferrite  $\text{Sr}_{1-x}\text{La}_x\text{Fe}_{11.80}\text{Cu}_{0.20}\text{O}_{19}$  magnets measured at room temperature; (a)  $x = 0.24$  and (b)  $x = 0.32$ .

$\text{La}_x\text{Fe}_{11.80}\text{Cu}_{0.20}\text{O}_{19}$  magnets is shown in Fig. 5. It is evident that  $(BH)_{\max}$  initially increases with  $x$  from 0.12 to 0.24, and then begins to decrease when  $x$  continues to increase. At  $x = 0.24$ ,  $(BH)_{\max}$  reaches to the maximum value of  $31.41 \text{ kJ/m}^3$ . The larger the maximum energy product is, the better the magnet is. Since the maximum energy product  $[(BH)_{\max}]$  is the maximum area in second quadrant of the hysteresis loop, the values of remanence ( $B_r$ ) and magnetic induction coercivity ( $H_{cb}$ ) will have their influence on it. From Fig. 4 and Fig. 5, the change of  $(BH)_{\max}$  has the same feature as that of  $H_{cb}$  as shown in Fig. 4.

Fig. 6 presents two typical demagnetizing curves for the hexaferrite  $\text{Sr}_{1-x}\text{La}_x\text{Fe}_{11.80}\text{Cu}_{0.20}\text{O}_{19}$  magnets measured at room temperature with La content ( $x$ ) of 0.24 and 0.32. As seen from Fig. 6(a), the magnet with  $x$  of 0.24 exhibits the magnetic properties, including the remanence ( $B_r = 413.3 \text{ mT}$ ), intrinsic coercivity ( $H_{cj} = 202.5 \text{ kA/m}$ ), magnetic induction coercivity ( $H_{cb} = 186.0 \text{ kA/m}$ ) and maximum energy product  $[(BH)_{\max} = 31.41 \text{ kJ/m}^3]$ . As seen from Fig. 6(b), the magnet with  $x$  of 0.32 shows the magnetic properties, including the remanence ( $B_r = 416.7 \text{ mT}$ ), intrinsic coercivity ( $H_{cj} = 153.8 \text{ kA/m}$ ), magnetic induction coercivity ( $H_{cb} = 150.5 \text{ kA/m}$ ) and maximum energy product  $[(BH)_{\max} = 29.71 \text{ kJ/m}^3]$ .

## Conclusions

Hexagonal ferrite  $\text{Sr}_{1-x}\text{La}_x\text{Fe}_{11.80}\text{Cu}_{0.20}\text{O}_{19}$  magnetic powders and magnets were synthesized according to the solid state reaction. X-ray diffraction was used to identify the phase compositions of the magnetic powders. There is a single magnetoplumbite phase in the magnetic powders with  $x$  from 0.12 to 0.32, and for the magnetic powders with  $x \geq 0.36$ , the  $\text{LaFeO}_3$  phase is observed. A field emission scanning electron microscopy was employed to investigate the microstructures of the magnets. The magnets are formed of hexagonal-shaped crystals and the particles are distributed evenly.

The magnetic properties of the magnets were measured by a magnetic properties test instrument.  $B_r$  of the magnets increases from 409.5 mT (at  $x = 0.12$ ) to 426.2 mT (at  $x = 0.40$ ). However,  $H_{cj}$  and  $H_{cb}$  of the magnets first increase from 176.2 and 165.6 kA/m (at  $x = 0.12$ ) to 202.5 and 186.0 kA/m (at  $x = 0.24$ ), respectively. With a further increase in the La content,  $H_{cj}$  and  $H_{cb}$  decrease drastically.  $(BH)_{\max}$  of the magnets first increases with  $x$  from 0.12 to 0.24, and then begins to decrease when  $x$  continues to increase.

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